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DEVICE FOR TRIGGERING A RESTRAINT SYSTEM

Background Information

The present invention is based on a device for triggering a restraint system according to the species defined in the independent claim.

5 From DE 199 09 538 A1, it is known to deploy the second airbag stage as a function of a criterion derived from the acceleration signal. DE 101 09 043 A1 describes triggering the second airbag stage as a function of two criteria derived from the acceleration signal.

Summary of the Invention

10 In contrast, the device of the present invention for triggering a restraint system having the features of the independent claim has the advantage that the second airbag stage is triggered on the basis of the closing velocity, determined using a precrash sensor system, and the deployment time of the first airbag stage. This has the advantage that the deployment time for the second airbag stage may be determined exactly.

15 The measures and refinements specified in the dependent claims allow for advantageous improvements to the device for triggering a restraint system set forth in the independent claim.

It is particularly advantageous that the at least one criterion, ascertained through a variable derived from the acceleration signal, is the deployment time for the first
20 airbag stage. Consequently, the second airbag stage is then determined as a function of the deployment time for the first airbag stage and the closing velocity. The deployment of the second stage is therefore calculated from that of the first stage plus the delay to be computed. To ascertain this delay, at least one class can be defined as a function of the deployment time of the first stage and the closing velocity. The
25 classes describe the different delays. This method offers the advantage that only that threshold-value function must be set which is necessary for deploying the first airbag stage. This reduces development expenditure. In addition, computing power is saved, since after the first stage is deployed, no further signal processing is necessary for deploying the second stage. This computing power may then be made available for
30 deploying other restraint means. An important advantage is that the second airbag

stage may be deployed precisely in relation to the first airbag stage. That is to say, both the minimum delay necessary, for example, for the deployment technique, and the maximum delay for the effective protection of the passengers may be adhered to precisely, since two threshold-value functions that are independent of each other are no longer used. It is also advantageous that the second airbag stage is never triggered at a closing velocity below a certain limit, e.g. 29 km/h. Thus, it is finally possible to fulfill the precise differentiation between the deployment of the first and the second stage necessary for the American legislation (FMVSS 208).

The lower limit is an empirical limiting value which indicates a lesser crash severity, so that the restraint force by the second airbag stage is not necessary here. Finally, it is also advantageous that the device defines at least three classes which are defined as a function of the closing velocity and the deployment time for the first airbag stage.

Brief Description of the Drawing

Exemplary embodiments of the present invention are shown in the drawing and are explained in detail in the following description.

Figure 1 shows a block diagram of the device according to the present invention;

Figure 2 shows a first flowchart;

Figure 3 shows a second flowchart;

Figure 4 shows a third flowchart;

Figure 5 shows a fourth flowchart; and

Figure 5 shows a classification.

Description

The object of the device according to the present invention is to precisely deploy the second airbag stage. To this end, the deployment time for the second airbag stage is determined as a function of a criterion, which was derived from the acceleration signal, and the closing velocity which was ascertained by a precrash sensor. The deployment time for the first airbag stage is used here in particular as the criterion.

Figure 1 shows the device according to the present invention in a block diagram. An acceleration sensor 42 is connected to a first data input of a control unit 43. A precrash sensor 41 for ascertaining the closing velocity is connected to a second data input of control unit 43. The algorithm for a restraint system 45, which here triggers a two-stage airbag, runs on a processor 44 in control unit 43. Control unit 43 is connected via a data output to restraint system 45, here, for example, to a two-stage airbag. However, it is clear that there are at least two two-stage airbags in restraint system 45 in a vehicle, one for the driver and one for the front-seat passenger. Further restraint means such as seat-belt pretensioners, or single-stage or multi-stage airbags are not shown here for the sake of simplicity.

Acceleration sensor 42 may be situated in control unit 43 or else mounted externally as a so-called satellite or peripheral acceleration sensor such as an upfront sensor or a side-impact sensor. Precrash sensor 41 is usually remote from control unit 43 and may take the form of a radar, ultrasound or video sensor for monitoring the surrounding field. Sensors 41 and 42 may be equipped with a signal-processing unit, and therefore already preprocess the ascertained measured values. The connection in control unit 43 may be implemented via a bus or via individual two-wire lines which are either uni-directional or bi-directional. Generally, only one uni-directional connection is necessary from sensor 41 or 42 to control unit 43. However, a bi-directional connection may also be useful for testing the individual sensors. More than sensors 41 and 42 shown here can be connected to control unit 43.

Figure 2 shows the first method. In the first method, the calculation of the deployment time of second stage 14 is based on the deployment time of first stage 11 and the further pattern of acceleration signal 12. If, for example, the first stage is deployed very early, the second stage is deployed with minimal delay, since in this case one must assume a very hard crash. If the first stage is first deployed later, then the acceleration signal must be observed further to decide whether it is a crash of such severity that the second stage must be deployed.

Figure 3 shows a second method. In the second variant, both acceleration signal 22 and closing velocity 21 are evaluated. In this context, the acceleration signal is processed. This may be, for example, a simple or double integration. The variable thus obtained is compared to a threshold which may be a function both of time and of velocity. If the threshold is exceeded, the second airbag stage is deployed.

Figure 4 shows a flowchart of the method which is executed in the device according to the present invention. The deployment time for first airbag stage 31 was already calculated by processor 44 using a signal from acceleration sensor 42. In addition, at this point, precrash sensor 41 has determined closing velocity 32. These two parameters enter into deployment algorithm 33 which is computed by processor 44. The result is the deployment time for the second airbag stage. It is labeled by reference numeral 34.

As Figure 5 shows, in addition to closing velocity 51, acceleration signal 52 determined by acceleration sensor 42 is used as an input parameter in the algorithm. This algorithm is processed in control unit 43. From these two parameters, in an algorithm (not further discussed here), with the aid of a signal processing 53, the deployment decision for the airbag with regard to the first stage is initially ascertained. For example, this may be accomplished either directly from the acceleration signal or via the velocity signal calculated by simple integration, or via forward-displacement signal 54 ascertained by double integration, by a threshold-value comparison 55. In this context, closing velocity 51 of precrash sensor 41 is also taken into account. In second step 56, from the deployment time for the airbag with respect to the first stage and from the closing velocity, the deployment decision is then calculated for the airbag in regard to the second stage. This is again carried out in two steps. To that end, first of all delay class 57, and therefore then in the second step, delay 58 itself is ascertained. The definition of a delay class is clarified in Figure 5. Here, closing velocity 60 is plotted over the deployment time of the airbag of first stage 69. For example, if the closing velocity is less than 29 km/h 67, then the airbag of the second stage must never be deployed. This is then case 68. If the velocity is above this limit, the second stage must be deployed with a certain delay. This is found in class 65. Here, for example, this applies to value pair 64. The delay may either be fixed or a function of the crash severity.

If, for example, the closing velocity is high, e.g. approximately 56 km/h, and the deployment time for the airbag of the first stage is very low, e.g. 8 ms, then one may assume a very severe crash - this pertains to value pair 62 - and the second stage must be deployed with a small delay. This then pertains to all value pairs for class 61. In the case of a slower crash, e.g. 40 km/h, with a later deployment time of the airbag with respect to the first stage, e.g. 45 ms - this pertains to the case of value pair 64 addressed above - the airbag must be deployed with a longer delay. Crash situations in

which the deployment of the second stage is delayed according to the same rule are combined to form delay classes.

Three such delay classes 61, 63, 65 are shown in Figure 6. However, to be delayed according to the same rule can also mean, for instance, that the delay time increases in linear fashion with the deployment time of the first stage or with the closing velocity. The separating lines between the individual delay classes may be established, for example, using a mathematical function or via a polyline defined by interpolation points. The number of delay classes can be a matter of choice, but at least one, so that in the simplest case, differentiation is only made between deployment and non-deployment.

Thus, given knowledge of the closing velocity and the deployment time of the first stage of the airbag, this method makes it possible to precisely ascertain the delay until the deployment of the second airbag stage.